

where

$$m = 4\pi/\alpha \quad (99)$$

If  $N_s$  is the number of segments then  $m = 2N_s$ .

The shear force  $\tau_{r\theta}$  must balance the pin force  $P$  shown in Figures 80 and 81. From Figure 80, it is seen for equilibrium of  $P$ , that it is required

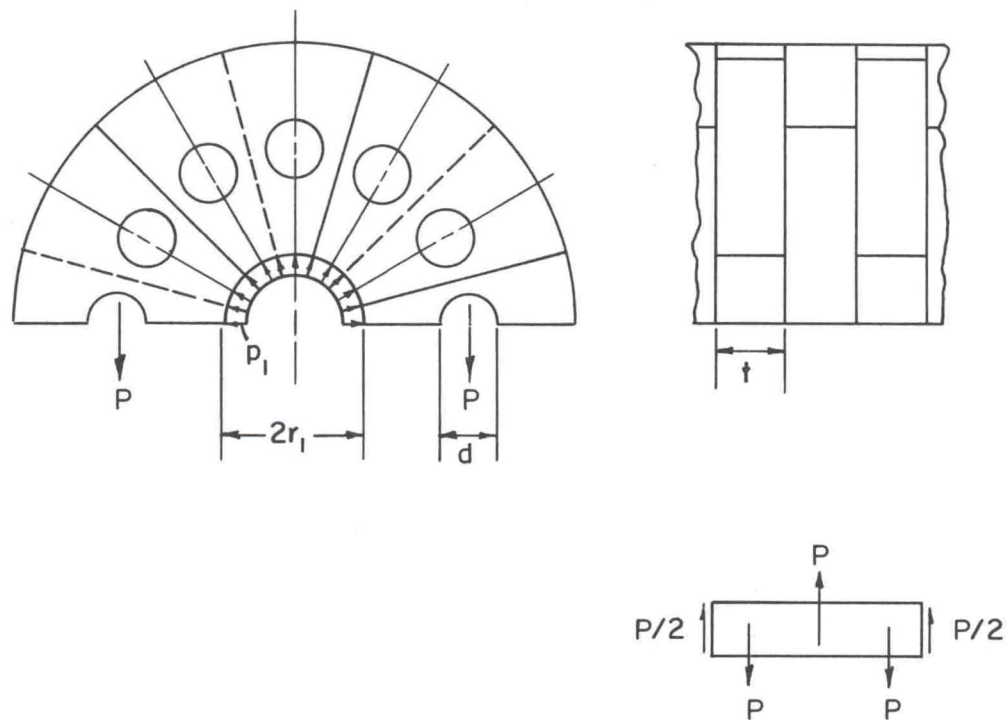
$$t \int_{\alpha/4}^{\alpha/2} \tau_{r\theta} \cos \left( \theta - \frac{\alpha}{4} \right) r_2 d\theta = P/2$$

where  $t$  is the segment thickness. Substitution of (98c) into this integral and integration gives

$$\tau = \frac{(m^2 - 1) P}{2mtr_2 (1 + \cos \pi/m)} \quad (100)$$

where  $P$  must be in equilibrium with  $p_1$  as shown in Figure 81, i. e.,

$$P = p_1 r_1 t \quad (101)$$



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FIGURE 81. LOADING OF PINS

For radial equilibrium of the loadings shown in Figure 80,  $p_2$  can be found by integration, i. e.,

$$2 \int_0^{\alpha/2} [\tau_{r\theta} \sin \theta - \sigma_r \cos \theta] r_2 d\theta \Big|_{r_2} = 2p_1 r_1 \sin \frac{\alpha}{2} .$$

Substitution for  $\tau_{r\theta}$  and  $\sigma_r$  from (98b, c) and integration gives

$$p_2 = \frac{1}{(m^2-2)} \left[ (m^2-1) \frac{p_1}{k_2} - m\tau \right] . \quad (102)$$

The stresses in a pin segment are found by superposition of three solutions: the Lamé solution for constant pressures  $p_1$  and  $p_2$  at the  $r_1$  and  $r_2$  respectively, a sinusoidal solution for the variable  $\sigma_r$  loading  $-p_2 \cos m\theta$  at  $r_2$ , and a bending solution to remove the hoop stress of the first two solutions from the sides of the segments. The Lamé solution is given by Equations (13a-c) and (14a, b) in the text. The sinusoidal solution, taken from the  $\cos m\theta$  part of Equation (81) in Timoshenko and Goodier<sup>(41)</sup>, is

$$\begin{aligned} \sigma_r &= \left[ m(1-m)a_m \rho^{m-2} + (2-m)(1+m)b_m \rho^m \right. \\ &\quad \left. - m(m+1)c_m \rho^{m-2} + (2+m)(1-m)d_m \rho^{-m} \right] \cos m\theta \\ \sigma_\theta &= \left[ m(m-1)a_m \rho^{m-2} + (m+2)(m+1)b_m \rho^m \right. \\ &\quad \left. + m(m+1)c_m \rho^{-m-2} + (m-2)(m-1)d_m \rho^{-m} \right] \cos m\theta \\ \tau_{r\theta} &= m \left[ (m-1)a_m \rho^{m-2} + (m+1)b_m \rho^m - (m+1)c_m \rho^{-m-2} \right. \\ &\quad \left. + (-m+1)d_m \rho^{-m} \right] \sin m\theta \end{aligned} \quad (103a-c)$$

where

$$\rho \equiv r/r_2 . \quad (104)$$

From the boundary conditions  $\sigma_r = 0$ ,  $\tau_{r\theta} = 0$  at  $r_1$  and  $\sigma_r = -p_2 \cos m\theta$ ,  $\tau_{r\theta} = -\tau \sin m\theta$  at  $r_2$  for the sinusoidal solution, the constants  $a_m$ ,  $b_m$ ,  $c_m$ , and  $d_m$  are found to be

$$\begin{aligned} a_m &= \left( \frac{-p_2}{2} + \frac{\tau}{2} \right) \left[ \frac{m^2 + (1-m^2)k_2^2 - k_2^{2m+2}}{\beta_2(m-1)} \right] \\ &\quad + \left( \frac{-p_2}{2} - \frac{\tau}{2} \right) \frac{k_2^2(1-k_2^{2m})}{\beta_2} \end{aligned}$$